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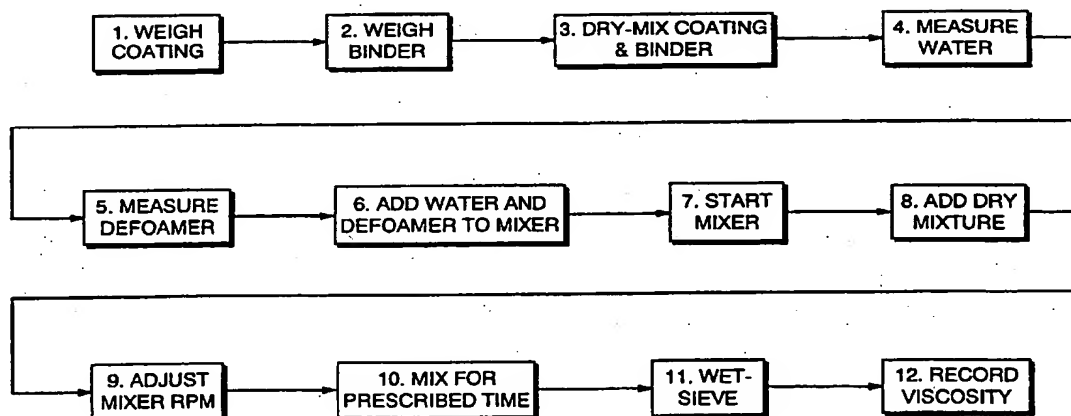
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(54) Title: **RELEASE COATING SYSTEM FOR CRUCIBLES**



(57) Abstract: A method for preparing a release coating and applying it to crucibles used to contain molten material while it solidifies, by mixing a release coating powder with a dry organic binder into a powder and binder dry mixture, mixing a defoamer with a liquid into a liquid and defoamer mixture, mixing the dry mixture with the liquid and defoamer mixture into a wet release coating, sieving to remove lumps and particles, checking the viscosity, wet-spraying onto a crucible, evaporating the liquid from the wet release coating so as to leave a dry release coating on the crucible, and separating the binder from the dry release coating by thermal decomposition.

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RELEASE COATING SYSTEM FOR CRUCIBLES

This application relates and claims priority for all purposes to pending US applications ser. no. 60/248880 filed on 11/15/2000 and serial no. 60/249023 filed on 11/15/2000

FIELD OF INVENTION

The invention relates to preparation and application of release coatings for crucibles used in the handling of molten materials that are solidified in the crucible and then removed as ingots, and more particularly to release coatings for crucibles used in the directional solidification of polycrystalline silicon.

BACKGROUND

Crucibles of fused-silica (quartz) are typically used in directional solidification of polycrystalline silicon. Quartz is chosen primarily for high-purity and availability. There are problems in using quartz, however, as a crucible for the production of silicon by this method.

Silicon in its molten state will react with the quartz crucible that is in contact with it. Molten silicon reacts with quartz to form silicon monoxide and oxygen. Oxygen will contaminate the silicon. Silicon monoxide is volatile, and will react with the graphite components inside the furnace. Silicon monoxide reacts with graphite to form silicon carbide and carbon monoxide. The carbon monoxide will then react with the molten silicon, forming additional volatile silicon monoxide and carbon. Carbon will contaminate the silicon.

The reaction between quartz and silicon promotes adhesion of the silicon to the crucible. This adhesion, combined with a difference in coefficients of thermal expansion between the two materials, creates stress in the silicon ingot, causing it to crack on

cooling. It is known in the art that a release coating applied to the inside of the crucible in the area of contact with the ingot can prevent the reaction between silicon and quartz that leads to ingot contamination and cracking. To be effective, the release coating must prevent the silicon from reacting with the quartz crucible, and must not adversely
5 contaminate the silicon either by itself or from contaminants within it.

A variety of materials and techniques are described in the literature, which attempt to solve the problem of reaction and adhesion of the crucible in contact with molten material. For example, US4256530 by Schmid et al., suggests coating the outside of a
10 quartz crucible with a refractory material, to prevent reaction with adjacent carbon components. The coating does not contact the molten silicon. The method of preparing and applying the coating are, however, undisclosed.

US5431869 by Kumar, et. al., describes a multi-component release agent of silicon
15 nitride and calcium chloride for silicon processing using a graphite crucible. The silicon nitride coating is applied as a slurry in an organic binder and solvent. The method of preparation and application are largely undisclosed. It is suggested that the binder can be removed after the coating, but the details are undisclosed. The calcium chloride portion is introduced with the bulk silicon, rather than as a coating, to the silicon-nitride coated
20 crucible. The use of silicon nitride alone is described as unfavorable as a crucible coating for directional solidification of silicon.

US4741925 by Chaudhuri, et. al., describes a silicon nitride coating for crucibles applied by chemical vapor deposition at 1250 degrees Centigrade. US3746569 discloses
25 the pyrolysis formation of a silicon nitride coating on the walls of a quartz tube. The process requires application temperatures at least 800 degrees C, and tempering at 1250 degrees Centigrade. US4218428 by Schmid, et. al., describes a technique of forming a glass layer inside a silica crucible by rapid heating to prevent cracking of silicon during melt-processing.

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US3660075 by Harbur et al., discloses a coating of niobium carbide or yttrium oxide on a graphite crucible for melting fissile materials. The niobium carbide is applied by chemical vapor deposition, while the yttrium oxide is applied as a colloidal suspension in an aqueous inorganic solution. Details such as the method of preparation and
5 application are largely undisclosed. US3613633 by Anderson, describes a heated rotating crucible used to hold articles to be coated. The crucible facilitates the containment of an "evaporant" which coats the articles therein. The crucible itself is not, however, used to contain molten material.

10 Reference is made in "Liquid Encapsulated Bridgman (LEB) Method for Directional Solidification of Silicon Using Calcium Chloride", by P.S. Ravishankar, Journal of Crystal Growth, 94 (1989) 62-68, to the coating of a silica crucible with silicon nitride. However, no method is detailed for preparing and applying the coating. Furthermore, the resulting ingot quality using this coating is described as poor, due to
15 particle nucleation leading to poor grain-growth and low solar cell efficiency.

Saito, et. al., in "A Reusable Mold in Directional Solidification for Silicon Solar Cells", Solar Energy Materials, vol 9, (1983) pg 337-345, and in "A New Directional Solidification Technique for Polycrystalline Solar Grade Silicon", Conf. Record of 15th
20 PV Specialists Conference, 1981, p 576-580, describes a coating of silicon nitride powder which is brushed onto a quartz, silicon carbide coated carbon or silicon nitride sintered mold. The powder is suspended in an organic solvent, which is evaporated by heating. Methods of preparation and application are not detailed, except that the coating needs to be at least 150 microns thick.

25 Saito reports, "The [silicon nitride] powder was mixed together with a suitable amount of organic solvent, such as liquid polyvinylalcohol, to form a slurry. The slurry was coated by a brush on the inner crucible walls. Then, the crucible was heated in an air ambient at 600C for 30 minutes to burn out the organic solvent. The coated layer thus
30 obtained had good mechanical strength against scratching." However, no method is

detailed for preparing and applying the coating. Brushing, we have found, is a difficult way to obtain a uniform coating.

Scaling a laboratory process such as Saito's up to production requirements is also problematic. Saito's crucible was only a few inches across, and contained only 225 g of molten material, while the present technology requires crucibles over two feet across, and contains over 240 kg of molten material. The difference in size and weight makes the physical demands on the coating and the coating process much more profound.

Other publications that mention crucible coatings, usually of silicon nitride, for directional solidification of silicon, but do not discuss methods of preparation or details of application, include: "HEM Technology for Photovoltaic Applications", Khattak et al, 6th IPSEC Conference, New Delhi, India, 1992, p 117-124; "Growth and Characterization of 200 kg Multicrystalline Silicon Ingots by HEM", 26th IEEE PVSC Conference, Anaheim, CA, Sep. 29-30 1997; "Growth of 240 kg Multicrystalline HEM Silicon Ingots", 2nd WCPEC Conference, Vienna, Austria, July 6-10 1998; "High Efficiency Solar Cells Using HEM Silicon", First WCPEC Conference, Dec 5-9, Hawaii, 1994 p 1351-1355; "Characteristics of HEM Silicon in a Reusable Crucible", 23rd IEEE PV Specialists Conference, Louisville, KY, May 10-14, 1993, p 73-77; "Analysis and Control of the Performance-Limiting Defects in HEM-Grown Silicon for Solar Cells", Material Research Society Symposium Proceedings, 1995, v 378 p 767-776; "Lifetime Improvement of Multicrystalline Silicon", Habler et al., 14th EPVSE Conference, Barcelona, Spain, June 30- July 4, 1997, p 720-723; "3D Distribution Study of Impurities into a Polix Ingot", Borne et al., 13th European PV Conference, Nice, France, 1995, p 1340-1343; "Study and Conditioning of Defect Areas in Eurosil Multicrystalline Silicon", Acciarri et al., 13th European PV Conference, Nice, France, 1995, p 1336-1339; and "Selection of a Crucible Material in Contact with Molten Silicon", Revel et al., 5th EC PV SEC, Athens, Greece, Oct. 17-21 1983, p 1037-1042.

Prior art references include specific references to powdered mold release agents for application to crucibles in the directional solidification of silicon. In addition, the use of

chemical vapor deposition, solvent evaporation, high-temperature flame treatment, and other expensive and complex means are mentioned for application of crucible coatings. References are made to specific binders and solvents. Although there is a tremendous emphasis in the literature on controlling the purity of the molten material, such emphasis is lacking in the prior art references as to the powder coating process. Silicon Nitride, for example, is available in a variety of phases, purity, and particle size, which may or may not make them suitable for coating.

References are made to mixing, spraying, or brushing for slurries of powdered coatings. There is no mention, however, of a method to mix, spray, or brush the coating in such a way as to control physical properties such as viscosity, foam content, dispersion quality, in order to provide a uniform coating on the crucible and to avoid contaminating the coating in the process of carrying out these steps.

We have discovered, for example, that the use of a specific silicon nitride powder, Baysinid(R), disclosed by Habler et al., in "Lifetime Improvement of Multicrystalline Silicon", 14th EPVSE Conference, Barcelona, Spain, June 30- July 4, 1997, p 720-723, in preparing crucible coatings, is heavily aggregated and difficult to disperse, created a poor suspension which was unstable, and caused spraying equipment to clog. This resulted in an extended time required for coating application, and a non-uniform coating which is not reliable in preventing adhesion of molten silicon to the crucible. Ingots were sometimes cracked during operations in which this material was used, due to difficulties related to poor dispersion and clogging. Milling operations using conventional means to properly grind the aggregates to form a stable suspension would contaminate the coating with metal or metal oxide that would contaminate molten silicon.

These examples illustrate how the reviewer of the prior art is led to believe that the selection of specific components and details of their preparation are obvious. We have found, however, that the selection of powders, binders, solvents, and their preparation for applying as a reliable and high-quality coating to a crucible is not in fact obvious, but requires substantial inventiveness to accomplish.

SUMMARY OF THE INVENTION

It is an object of this invention to provide a simple, inexpensive coating system
5 and application process for coating crucibles with a release coating for use in a production
environment for the manufacture of ingots of polysilicon or other materials. The system
will preferably include a coating material having suitable crucible adhesion and ingot
release characteristics when applied to a crucible as a release layer for the molten material,
and for which there is a powdered form of the material available with a suitable particle size
10 and dispersibility for spray application using commercial equipment and conventional
methods.

There will be a safe and inexpensive liquid solvent for the coating material,
preferably water, in which to suspend the powder, and an organic binder possessing
15 physical and chemical characteristics that facilitate the application of the coating system to
crucibles using commercially available spraying equipment. The coating may include
additives to improve its quality, make it more sprayable, easier to apply uniformly, and
improve its mixing characteristics and control its physical properties. The powder, binder,
and solvent are selected and processed such that the resulting final release coating on the
20 crucible does not adversely contaminate the molten material.

It is a further object of the invention to provide a means to remove the solvent from
the coating and harden the binder to prevent movement of the coating during subsequent
25 processing, such as by preheating or holding the crucible at a slightly elevated temperature
so as to facilitate the evaporation of the solvent and drying of the coating on the crucible
after the spraying operation.

It is another object to provide a means to remove the binder by thermal
30 decomposition from the coating and to densify the final coating so as to minimize damage
to the coating during subsequent processing of the molten materials, such as by bisque-

firing the crucible by slowly heating the crucible in oxidizing air to well above a temperature at which the binder material will be readily oxidized dispersed into the air, maintaining the crucible at or near that temperature for a period of time to assure hardening of the remaining layer, and allowing it to cool slowly to room temperature.

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Still other objects and advantages of the present invention will become readily apparent to those skilled in this art from the following detailed description, wherein we have shown and described only a preferred embodiment of the invention, simply by way of illustration of the best mode contemplated by we on carrying out our invention.

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BRIEF DESCRIPTION OF THE FIGURES

Fig. 1 is a flowchart of the steps of the preferred embodiment method of the invention as described below.

Fig. 2 is a simplified block diagram of the materials flow of the flowchart of Fig. 1.

DESCRIPTION OF THE PREFERRED EMBODIMENT

The material to be applied as a crucible release coating is provided in powder form and is readily dispersible in water by high-speed mixing. Readily dispersible refers to a suspension, once prepared at the correct viscosity, which can be applied as a uniform coating by commercially-available spray-painting equipment without clogging, and from which particles will not segregate by settling during the time period required for application to the crucible. Such a suspension will exhibit no scratches when tested using a 50 micron Hegman Gauge. High-speed mixing refers to using a shaft mixer with a non-metal or non-metal coated dispersion blade of the "cowles" design or equivalent, such as Norstone(tm). The peripheral speed of the mixing blade is maintained at or above 3000 revolutions per minute, such that the vortex formed by the liquid exposes not less than two thirds (2/3) of the diameter of the mixing blade.

Referring to Figure 1, a logic flowchart depicting the steps of the process to prepare the coating, the coating powder is weighed (1) and combined with an appropriate weight (2) of dry water-soluble polymer binder material such as cellulose ether. The ratio of coating powder to binder is at least 5:1 weight basis. The coating powder and binder are mixed together (3) into a dry mixture until the binder is indistinguishable from the coating powder by visual inspection.

Deionized water having an electrical resistivity greater than 10,000 ohm-cm is measured (4) and poured into a clean plastic or plastic-lined vessel having a volume

sufficient to contain the wet coating during preparation. Added to the water is a defoamer (5), such as Polyglycol P1200 polypropylene glycol or equivalent, in the amount of 500 - 1000 ppm for the volume of water used. Absence of defoamer in the process results in large amounts of foam produced, which will reduce dispersion efficiency, markedly increase the volume and viscosity of the suspension, and reduce the smoothness of the sprayed coating on the crucible.

The water and defoamer mixture are added to the mixer (6) and agitated (7) as described above. While mixing, the dry mixture is added slowly (8) to the water, forming a wet coating. The mixer speed is adjusted (9) during dry mixture addition to maintain the vortex of the liquid. Mixing is continued (10) after dry mixture addition is completed, for a prescribed period of time necessary for the wet coating viscosity to equilibrate. After mixing is completed, the wet coating is sieved (10) through a fine-mesh paint bag, into a clean, dry beaker and its viscosity is recorded (12).

After mixing, the wet coating is transferred to a commercially available spray gun such as Binks 95G. The crucible to be coated for release is prepared for coating by heating to a temperature above 110F and less than 150F by heating in an oven, or by heat-lamps or heat-guns, or by direct contact heating with heat blankets, or other convenient means, thereby facilitating rapid drying of the coating. The wet coating is sprayed evenly onto the surface of the crucible at a rate sufficient to prevent running, or cracking upon drying. Once coated, the wet coating is permitted to dry to form a dry release coating. If a thicker coating is required the crucible is reheated as before and the coating is applied again and permitted to dry.

The dry release coating is then transferred to a kiln which will heat the crucible to a temperature necessary to remove the binder by thermal decomposition in oxidizing air, and to partially densify the coating to a "bisque-fired" condition. An oxidizing atmosphere is required, otherwise the organic material will decompose to carbon, which may cause contamination of the molten material during directional solidification. The crucible is then cooled to a temperature where it can be handled by an operator. The finished crucible is

then removed. The strength of the coating is sufficient after firing to maintain coating integrity during loading and manipulation of the crucible into the furnace.

Referring to Fig. 2, a diagrammatic illustration of the materials path of the process correlating to the Fig. 1 steps of the process, coating power A and binder B are weighed and dry mixed together in container 20 at a minimum ratio of 5:1, dry mixture AB being mixed until binder B is indistinguishable from power A. Separately, in container 30, to the selected volume of deionized water C there is added the 500 - 1000 parts per million volume of defoamer D, the result being water/defoamer mixture CD. Then water/defoamer mixture CD is added to the high speed mixer 40 first, and the vortex agitation begun. Dry mixture AB is slowly added to mixer 40, with appropriate adjustments to mixer power and speed to maintain the vortex, thus forming the wet release coating ABCD.

Wet release coating ABCD is then passed through sieve 50, a fine mesh paint bag, and into beaker 60, where viscosity is checked. From there, the coating is transferred to spray gun 70, for conventional spray application to at least the interior of crucible 80, which is being maintained at a slightly elevated temperature by heat lamps 90. The wet release coating on the warm crucible dries quickly, evaporating the water component and leaving a dry release coating consisting substantially of power A and binder B.

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Crucible 80 with its dry release coating AB is then transferred to kiln 100, where the crucible is heated to a temperature necessary to remove binder B by thermal decomposition, leaving a final release coating A, and to partially densify the remaining release coating to a "bisque-fired" condition. Crucible 80 is then cooled and removed for use in the production of polysilicon.

25

As an example of the preferred method, 390 grams of silicon nitride powder (H.C. Stark, Newton, MA), having a volume average particle size of 0.7 microns, with 90 vol% less than 1.2 microns, and 10 vol% less than 0.5 microns, is thoroughly mixed in dry form with 72 grams of cellulose ether (Dow Chemical, Midland, MI) binder to form a dry mixture in a glass container using a Teflon rod. The silicon nitride powder has a level of

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iron less than 7 ppm, and copper 0.5 ppm. The binder has a viscosity in water of 15 centipoises at a concentration of 2 wt%. The binder has iron at 20 ppm and copper 0.5 ppm. Into another glass container of 2 liters capacity, 1500 ml of deionized water is mixed with 1 ml of polyglycol P1200 (Dow Chemical, Midland, MI) defoamer. The water and defoamer are mixed using a high-shear mixer. The mixer is fitted with a 3" diameter polyurethane impeller (Norstone, Inc.), and is operating at a speed capable of generating a vortex that covers only 1/3 the diameter of the impeller.

The dry mixture is added to the water mixture in 50 ml increments over a period of 10 minutes, to form a wet coating. The water is deionized and has a resistivity of greater than 17 megaohm-cm. During the addition, the speed of the mixer is adjusted to maintain the vortex, with 1/3 diameter or less impeller coverage. Once the dry mixture is added, the wet coating is mixed for 10 minutes to completely dissolve the binder. After mixing, the wet coating is removed from the mixer and poured slowly through a standard fine-mesh paint bag into a 2 liter glass beaker and allowed to de-air for 15 minutes. The paint bag trapped no lumps or grit particles.

The condition of the coating is a smooth suspension with no lumps or grit detectable when rubbed through the fingers. A sample is withdrawn to a standard Hegman gauge which confirms dispersion quality by displaying no scratches down to zero reading. The viscosity is tested using a Zahn #2 cup with a result of 60 seconds. The wet coating is sprayed using a spray gun (Binks, Inc. 95-G) onto a silica crucible heated to 120 - 150 Degrees F using a heat-lamp, and dried in air at 120 - 150 degrees F

During the spray process the coating is sprayed slowly and evenly to avoid runs or drips, in thin coats which are allowed to dry before reapplying. The dried coating is smooth with no cracks. The total application and drying time are 90 minutes. The coating is measured using a Durometer which reads 89 Shore A. The coated crucible is heated in air to 1095 degrees C over a period of 12 hours, maintained at 1095 degrees C for 3 hours, and allowed to cool slowly to room temperature. The coating is then measured with a durometer which shows it has been hardened to 95 Shore A.

The invention is susceptible of many variations, all within the scope of the claims that follow. For example, there is a method for preparing a wet release coating for spray application to crucibles used to contain molten material in a HEM furnace while it solidifies into an ingot. The crucible may be a fused-silica crucible, although other materials are and can be used for such crucibles. The molten material may be silicon or such other material as needs to be processed from a molten state to a hardened state within a crucible, cooled, and then removed. The wet release coating will need to be applied to the crucible by some suitable fashion, and may require further treatment or processing to reach a final state of readiness for use with the molten material.

There is first weighed a unit portion of a release coating power, that is to say a powdered form of the material that will be the finish coating on the crucible. Then there is measured out a corresponding portion of a dry organic binder, compatible with the coating material, of not more than one fifth by weight of the unit portion of release coating power. The binder is mixed with the coating power into a dry mixture.

There is measured out a unit volume of liquid solvent sufficient for the process. There is then measured out a corresponding unit volume of a defoamer compound of between about 500 to 1000 parts per million by volume of the unit volume of liquid. The defoamer is then mixed with the liquid into a liquid and defoamer solvent mixture. The dry mixture of power and binder are mixed with the liquid and defoamer mixture into a wet release coating, which is then sieved to remove lumps and particles. The wet coating may be checked for suitable viscosity prior to attempting its application.

The release coating may be a compound from among a group of compounds consisting of silicon nitride, silicon carbide, zirconium oxide, barium zirconate, magnesium zirconate, or a combination thereof. The organic binder may be cellulose ether. The cellulose ether may have a viscosity of not less than 15 centipoises at 20 degrees C, at a concentration in water of two percent. The ratio of the coating powder to the organic binder may be at least 5:1 by weight.

The liquid may be deionized water with an electrical resistivity of at least 10,000 megaohms-cms. The defoamer may consist of one of a group of defoamers that includes polypropylene glycol and polyethylene glycol.

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As another example, there is a method for applying a release coating, such as the wet release coating above, to crucibles used to contain molten material while it solidifies into an ingot, consisting of the further steps of wet-spraying the release mixture onto a crucible, evaporating the liquid from the wet release coating so as to leave a dry release
10 coating on the crucible, which may be done by heating the crucible in any convenient way so as to hasten the evaporation process, and then separating the binder from the initial dry release coating by thermal decomposition so as to leave a hardened finish release coating. As above, the crucible may be a fused-silica crucible, although other materials are and may be used for such crucibles. The molten material may be silicon or such other material
15 as need be processed from a molten state to a hardened state within a crucible, cooled, and then removed.

As yet another example of the invention, there is a method for applying a release coating to crucibles used to contain molten material, consisting of the steps of mixing a
20 release coating power with a dry organic binder into a powder and binder dry mixture, mixing a defoamer with a liquid solvent into a solvent mixture, mixing the dry mixture with the solvent mixture into a wet release coating, sieving the wet release mixture so as to remove lumps and particles to the degree required for the intended spraying equipment and technique, wet-spraying the release mixture onto a crucible, evaporating the solvent
25 mixture from the wet release coating so as to leave a dry release coating on the crucible, and then decomposing the binder from the dry release coating and hardening the finish release coating.

The decomposing of the binder is preferably done by thermal means such as slowly
30 raising the temperature of the sprayed crucible in air to or above the decomposition

temperature of the binder, so that the binder components are oxidized and dissipated in the air.

5 The crucible may be a fused-silica quartz crucible. The molten material may be silicon. The organic binder may be cellulose ether. The cellulose ether may have a viscosity that is not less than 15 centipoises at 20 degrees C, at a concentration in water of two percent.

10 The release coating may be a compound from among the group of compounds consisting of silicon nitride, silicon carbide, zirconium oxide, barium zirconate, magnesium zirconate or combinations of these. The wet release coating may have a ratio by weight of powder to organic binder of at least 5:1. The liquid solvent may be deionized water with an electrical resistivity of at least 10,000 megaohms-cms. The dry release coating having a particle size 90% by volume less than 2 microns in diameter.

15 The defoamer may be one of a group of defoamers consisting of polypropylene glycol and polyethylene glycol. The wet release coating may have a viscosity as measured by Zahn#2 cup of between 15 and 120 seconds, preferably between 50 and 80 seconds. The step of decomposing may consist of slowly heating the crucible to at least the thermal decomposition temperature of the binder.

20 There may be, prior to the step of wet-spraying, the further step of assuring the viscosity of wet release mixture is suitable for spray application. This means first, simply measuring the viscosity to assure that it is within the desired range for the intended spraying equipment and technique. If upon measuring the viscosity, it is found to be out of range, further adjustment of the ratio of dry mixture to solvent mixture is made by adding one or the other to the wet release mixture as needed, mixing or remixing as before, re-sieving the mixture, and rechecking the viscosity. This is repeated, if necessary, until the viscosity is within an acceptable range for the spraying operation.

As yet another example of the invention, there is a method for applying a release coating to crucibles used to harden molten material into ingots, consisting of the steps of weighing a unit portion of a release coating power, measuring out a corresponding portion of a dry organic binder of not more than one fifth by weight of the unit portion of release
5 coating power, mixing the binder with the power into a dry mixture, measuring a unit volume of liquid solvent, and measuring out a corresponding unit volume of a defoamer of between about 500 to 1000 parts per million by volume of the unit volume of liquid solvent, mixing the defoamer with the liquid solvent into a solvent mixture.

10 Then, mixing the dry mixture with the solvent mixture into a wet release coating, sieving the wet release mixture so as to remove lumps and particles to the degree required for the intended spraying equipment and technique, assuring proper viscosity of the wet release mixture for spraying, wet-spraying the release mixture onto a said crucible, evaporating the solvent mixture from the wet release coating so as to leave a dry release
15 coating on the crucible, and separating the binder from the dry release coating by thermal decomposition.

As still yet another example of the invention, there is a method for preparing a wet release coating for spray application to a crucible used to contain molten material while it
20 cools into an ingot, consisting of the steps of weighing a unit portion of a release coating power, measuring out a corresponding portion of a dry organic binder of not more than one fifth by weight of the unit portion of release coating power, mixing the binder with the power into a dry mixture, measuring a unit volume of liquid solvent, measuring out a
25 corresponding unit volume of a defoamer of between about 500 to 1000 parts per million by volume of the unit volume of liquid solvent, mixing the defoamer with the liquid solvent into a solvent mixture, mixing the dry mixture with the solvent mixture into a wet release coating, sieving the wet release mixture so as to remove lumps and particles, and assuring viscosity of wet release mixture is suitable for spray application.

As will be realized, the invention is capable of other and different embodiments, and its several details are capable of modifications in various obvious respects, all without departing from the invention.

CLAIMS

We claim:

- 5 1. A method for applying a release coating to crucibles used to form molten material into a solid ingot, comprising the steps:
- mixing a release coating power with a dry organic binder into a powder and binder dry mixture,
- mixing a defoamer with a liquid solvent into a solvent mixture,
- 10 mixing said dry mixture with said solvent mixture into a wet release coating, sieving said wet release mixture so as to remove lumps and particles, wet-spraying said release mixture onto a said crucible, evaporating said solvent mixture from said wet release coating so as to leave a dry said release coating on said crucible,
- 15 decomposing said binder from said dry release coating.
2. A method for applying a release coating according to claim 1, said crucible being a fused-silica crucible.
- 20 3. A method for applying a release coating according to claim 1, said molten material being silicon.
4. A method for applying a release coating according to claim 1, said organic binder being cellulose ether.
- 25 5. A method for applying a release coating according to claim 4, said cellulose ether having a viscosity of not less than 15 centipoises at 20 degrees C, at a concentration in water of two percent.

6. A method for applying a release coating according to claim 1, said release coating comprising a compound from among the group of compounds consisting of silicon nitride, silicon carbide, zirconium oxide, barium zirconate, magnesium zirconate.

5 7. A method for applying a release coating according to claim 1, the ratio by weight of said powder to said organic binder being at least 5:1.

8. A method for applying a release coating according to claim 1, said liquid solvent being deionized water with an electrical resistivity of at least 10,000 megohms-cms.

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9. A method for applying a release coating according to claim 1, said dry release coating having a particle size 90% by volume less than 2 microns diameter.

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10. A method for applying a release coating according to claim 1, said defoamer comprising one of a group of defoamers consisting of polypropylene glycol and polyethylene glycol.

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11. A method for applying a release coating according to claim 1, said wet release coating having a viscosity as measured by Zahn#2 cup of between 15 and 120 seconds, preferably between 50 and 80 seconds.

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12. A method for applying a release coating according to claim 1, said step of decomposing comprising slowly heating said crucible in oxidizing air to at least the thermal decomposition temperature of said binder.

13. A method for applying a release coating according to claim 1, further comprising prior to said step of wet-spraying the step:

assuring viscosity of said wet release mixture is suitable for spray application.

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14. A method for applying a release coating to crucibles used to form molten material into a solid ingot, comprising the steps:

weighing a unit portion of a release coating power,
measuring out a corresponding portion of a dry organic binder of not more than one
fifth by weight of said unit portion of release coating power,
mixing said binder with said power into a dry mixture,
5 measuring a unit volume of liquid solvent,
measuring out a corresponding unit volume of a defoamer of between about 500 to
1000 parts per million by volume of said unit volume of liquid solvent,
mixing said defoamer with said liquid solvent into a solvent mixture,
mixing said dry mixture with said solvent mixture into a wet release coating,
10 sieving said wet release mixture so as to remove lumps and particles,
assuring viscosity of said wet release mixture is suitable for spray application,
wet-spraying said release mixture onto a said crucible,
evaporating said solvent mixture from said wet release coating so as to leave a dry
said release coating on said crucible,
15 separating said binder from said dry release coating by thermal decomposition.

15. A method for applying a release coating according to claim 14, said crucible being a
fused-silica crucible, said molten material being silicon.

20 16. A method for applying a release coating according to claim 15, said release coating
comprising a compound from among the group of compounds consisting of silicon nitride,
silicon carbide, zirconium oxide, barium zirconate, magnesium zirconate.

25 17. A method for applying a release coating according to claim 16, said organic binder
being cellulose ether having a viscosity of not less than 15 centipoises at 20 degrees C, at a
concentration in water of two percent, the ratio by weight of said powder to said organic
binder being at least 5:1.

30 18. A method for applying a release coating according to claim 14, said liquid solvent
being deionized water with an electrical resistivity of at least 10,000 megaohms-cms, said

defoamer comprising one of a group of defoamers consisting of polypropylene glycol and polyethylene glycol.

19. A method for applying a release coating according to claim 14, said wet release coating
5 having a viscosity as measured by Zahn#2 cup of between 15 and 120 seconds, preferably between 50 and 80 seconds, said dry release coating having a particle size 90% by volume less than 2 microns diameter.

20. A method for preparing a wet release coating for spray application to crucibles used
10 to contain molten material, comprising the steps:
weighing a unit portion of a release coating power,
measuring out a corresponding portion of a dry organic binder of not more than one
fifth by weight of said unit portion of release coating power,
mixing said binder with said power into a dry mixture,
15 measuring a unit volume of liquid solvent,
measuring out a corresponding unit volume of a defoamer of between about 500 to
1000 parts per million by volume of said unit volume of liquid solvent,
mixing said defoamer with said liquid solvent into a solvent mixture,
mixing said dry mixture with said solvent mixture into a wet release coating,
20 sieving said wet release mixture so as to remove lumps and particles,
assuring viscosity of said wet release mixture is suitable for spray application.

21. A method for preparing a wet release coating according to claim 20, said release
coating comprising a compound from among the group of compounds consisting of silicon
25 nitride, silicon carbide, zirconium oxide, barium zirconate, magnesium zirconate.

22. A method for preparing a wet release coating according to claim 20, said organic
binder being cellulose ether having a viscosity of not less than 15 centipoises at 20 degrees
C, at a concentration in water of two percent, the ratio by weight of said powder to said
30 organic binder being at least 5:1.

23. A method for preparing a wet release coating according to claim 20, said liquid solvent being deionized water with an electrical resistivity of at least 10,000 megaohms-cms.
- 5 24. A method for preparing a wet release coating according to claim 23, said defoamer comprising one of a group of defoamers consisting of polypropylene glycol and polyethylene glycol.
- 10 25. A method for preparing a wet release coating according to claim 20, said wet release coating having a viscosity as measured by Zahn#2 cup of between 15 and 120 seconds, preferably between 50 and 80 seconds, said dry release coating having a particle size 90% by volume less than 2 microns diameter.

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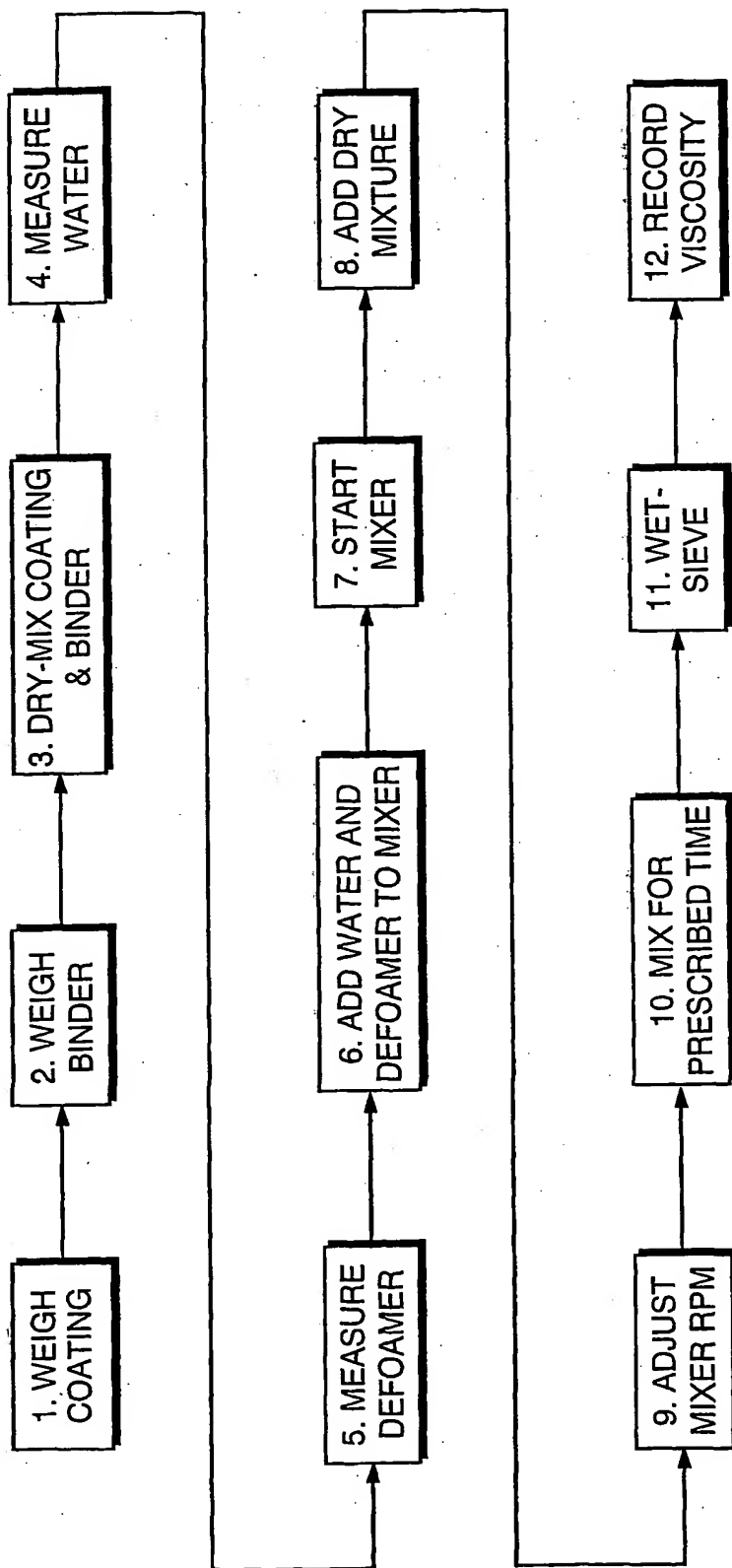


FIG. 1

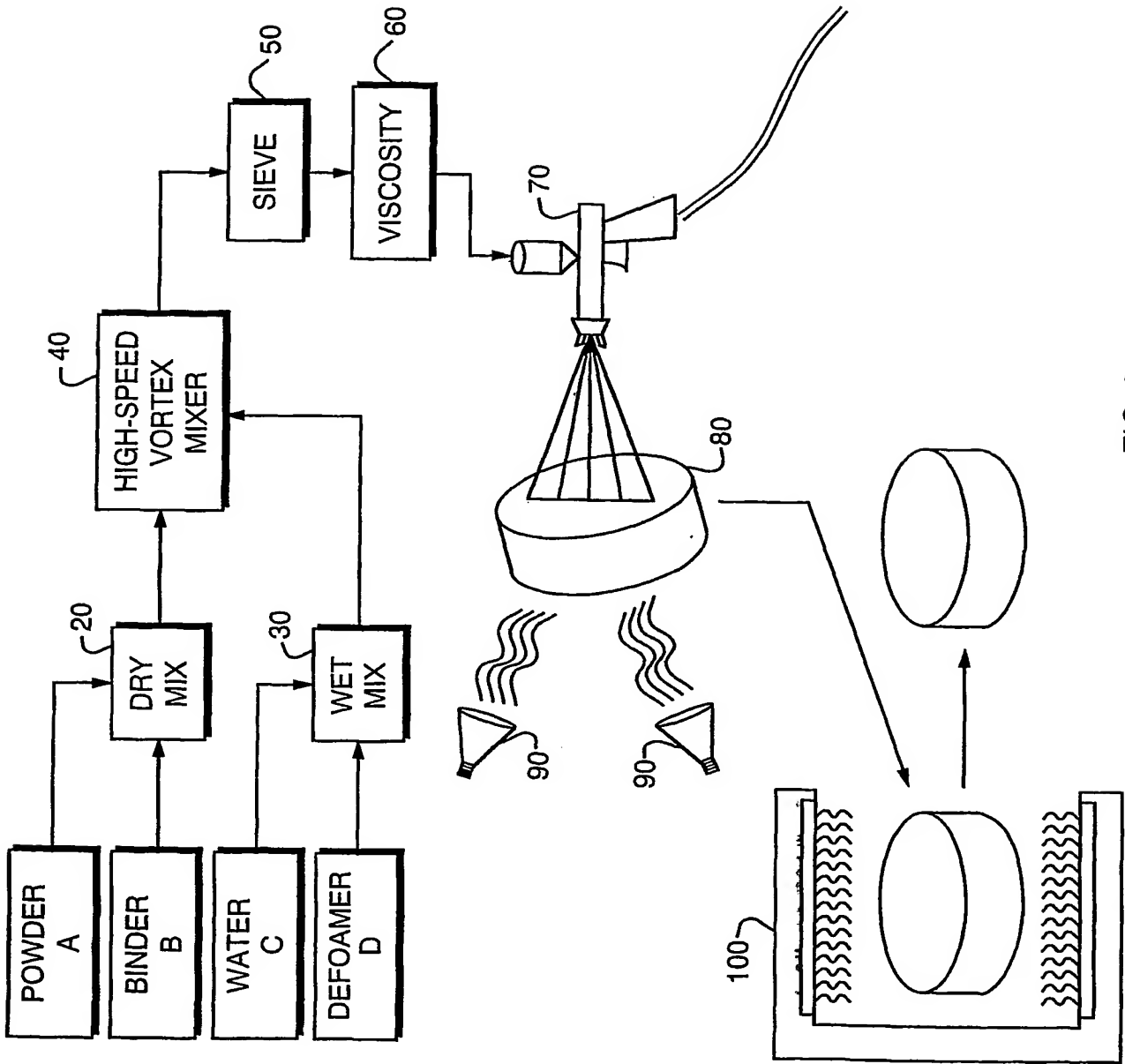


FIG. 2

INTERNATIONAL SEARCH REPORT

International application No.

PCT/US01/11830

A. CLASSIFICATION OF SUBJECT MATTER

IPC(7) : B05D 3/02, 7/22

US CL : 427/226, 236

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 427/226, 236

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
EAST search terms: release coating, crucible, binder, defoamer**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 5,431,869 A (KUMAR et al) 11 July 1995 (11.07.1995), whole document.	1-25
Y	US 5,384,291 A (WEIMER et al) 24 January 1995 (24.01.1995), col. 3-5.	1-25
Y	US 5,540,884 A (CHIAO) 30 July 1996 (30.07.1996), col. 4.	1-25

☐ Further documents are listed in the continuation of Box C.☐ See patent family annex.

* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier application or patent published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

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- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
- "&" document member of the same patent family

Date of the actual completion of the international search

06 July 2001 (06.07.2001)

Date of mailing of the international search report

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